# Reconfiguring Low Voltage Networks To Increase Voltage And Loss Of Electricity

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**Abstract**: In the operation of the electric power system, a good quality and level of reliability is needed, one of which is that the voltage that reaches the customer does not experience a voltage drop below the standardization from PLN. The voltage drop regulation according to SPLN No.72 of 1987 is the voltage drop on the Medium Voltage Network is a maximum of 5%, the voltage drop on the transformer is a maximum of 3%, the voltage drop on the Low Voltage Network is a maximum of 4%, and the voltage drop on the service line is a maximum of 1%. Brumbung Village, which is located in Mranggen District, Demak Regency, is one of the areas experiencing stress drop problems. The measured voltage at the Low Voltage Network subscriber location at the end of the day at 12.00 is 173 Volts, and at night when the peak load occurs at 19.00 is 154 Volts. With these conditions it is necessary to reconfigure the network in the area.

Network reconfiguration planning includes the addition of 10 new poles to get consumers closer to the voltage source, enlarging the network cable size, adding a 50KVA 1-phase distribution transformer, and reconfiguring house connections. After reconfiguring the network, the magnitude of the voltage drop simulation results from the ETAP voltage drop is 0.4% - 2.6% and the power loss is 1.1%, these results are in accordance with the SPLN, namely the allowable voltage drop does not exceed 5%, (SPLN 72, 1987).

Keywords: voltage drop, power loss, network repair.

#### I. INTRODUCTION

The electrical problem felt by the public is a voltage problem. One of the areas experiencing stress reduction problems is Brumbung Village, Demak Regency. The stress reduction on customers in this area exceeds the standards allowed in the SPLN. The measured voltage at the JTR customer location at the end of the day at 12.00 is 173V, and at night when the peak load occurs at 19.00 is 154V. With a very low voltage causes customer electronics to become damaged quickly. At 19.00 when there is a peak load, consumers cannot handle TV, TL lamps, radios, refrigerators and other electronic devices. The customer can only build an incandescent lamp but the flame is dim.

Based on the survey results, the network system is carried out radially with the number of draws at several location points exceeding the provisions allowed in the SPLN, namely the distance between the draws on the house channel exceeds 30 meters with the number of pulls exceeding 5 pieces. Meanwhile, according to the SPLN, the distance between the draws on the house channel (SR) does not exceed 30 meters with a maximum number of customer traps 5 pieces. The impact of this condition is the voltage drop or voltage drop received at the customer side, this is due to the large stress losses in the conductor due to the long pull.[4,5,6]

From this case the writer will calculate the amount of voltage and power loss (losses) generated and simulate it in the ETAP 12.6 software and plan network reconfiguration for problems in the area.[7,8]

#### II. RESEARCH METHODS

# 2.1 Low Voltage Network Voltage Drop

One of the criteria considered in designing a Low Voltage Network is the voltage drop. Based on SPLN No.72: 1987 the allowable voltage drop limits ( $\Delta$  V maximum) are as follows:

- 1.Drop Voltage on Medium Voltage Network = 5%
- 2.Drop Voltage on Transformer = 3%
- 3.Drop Voltage on Low Voltage Network = 4%
- 4. Voltage Drop on Service Line = 1%

The value of voltage drop ( $\Delta$  V) usually varies depending on load fluctuation. So that in order to optimize the network, the maximum value is taken according to SPLN No. 72: 1987.

To get the amount of voltage drop within this limit, the selection of the conductor used must consider the following:

- 1. Type of Conductor
- 2. The cross-sectional area of the conductor.
- 3. Network Length
- 4. Load density

In addition to the selection of the conductor used, it must be limited to the amount of load current that flows in accordance with the KHA (Current Conducting Capacity) of the type of conductor so that the allowable voltage drop limit can be achieved (Pusdiklat PLN, 2009: 43).

According to the Distribution Network Criteria Design book published by Pusdiklat PT.PLN (Persero) in 2009 on page 44, the type, area, and length of the conductor used for the JTR will affect the amount of impedance (Z) of the JTR. Multiplying the impedance Z with the current flowing will get the amount of voltage drop on the JTR, like the following formula:

$$\Delta V = \ I \ x \ Z \label{eq:deltaV}$$
 Information :

 $\Delta V = Voltage drop (Volt).$ 

I =The load current that flows (A).

Z = Impedance JTR (Ohm)

If the Low Voltage Network is represented as a diagram like the one above, then according to Kirchhoff's Law:

VS = VL + (R + j X). L = VL + RI + j X. IV drop = VS - VL = RI + j X. I= I(R + jX) Volt= Re (I Z)Where:

Real size  $Z = (R^2 + X^2)^{1/2}$ 

Information:

Z = Low Voltage Network Impedance (Ohm)

 $R = Conducting resistance (\Omega / km).$ 

 $X = Conducting Reactance (\Omega / km).$ 

#### 2.2 Losses

Losses are a form of loss of electrical energy that comes from the difference between the amount of available electrical energy and the amount of electrical energy sold. These losses are caused by two factors, namely technical factors in the form of network problems and non-technical factors, namely inaccuracy in recording, usage or in the calculation of kWh. In economic terms, losses are closely related to the problem of efficiency, so it can be concluded that the more inefficient, the smaller the profit from the income earned. The cost inefficiency that occurs in the flow of electrical energy is closely related to problems in terms of technology and the role of human resources,[16].

 $Losses = I^2 \times R \times I$ 

Presentase Losses:

% Losses = 
$$\frac{a}{b}$$
 x 100 %

Information:

a = value of losses (Watt)

b = feed power from the substation (Watt)

## 2.3 Figure of Existing Network of Case Study Sites

In the existing network that has been installed at the location of this case study, it is taken from the Morawa brand 50 KVA transformer which is connected to a low-voltage network (JTR) with a 2x35mm2 + N25 LVTC / NFA2X-T conductor which is then supplied to SLP using LVTC / NFA2X 2x16mm2 and distributed to houses use 2x10mm2 LVTC / NFA2X cables. The measured load on the transformer is 252 Ampere (OverBlast). On the existing network there are 121 consumers with an average power of 450VA (2 Ampere).

In the existing network there are 6 electric poles, namely pal T1-121 / 11, T1-121 / 11A, T1-121 / 11B, T1-121 / 11C, T1-121 / 12, and T1-121 / 13 with a distance approximately 40-50 meters. On pal T1-121 / 11 there are 3 external service channel pulls tapped directly from the low voltage network pole with a total of 9 outside service channels. On pal T1-121 / 11A there are 3 pulls. Outside service channels are tapped directly from the low voltage network pole with a total of 7 outside service channels. On pal T1-121 / 11B there are 3 pulls. Outside service channels are tapped directly from the low voltage network pole with a total of 7 outside service channels. On pal T1-121 / 11C there are 4 pulls. Outside service channels are tapped directly from the low voltage network pole with a total of 58 outside service channels. On pal T1-121 / 12, there are 5 pulls. Outside service channels are tapped directly from the low voltage network pole with a total of 15 outside service channels. On pal T1-121 / 13 there are 5 pulls. The outside service channel is tapped directly from the low voltage network pole

With a total of 25 outside service channels

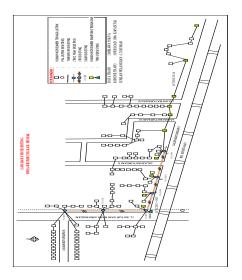


Figure 1 Image of Existing Network

#### 2.4 Existing Network Data of Case Study Sites

In calculating both the power loss calculation and the voltage drop calculation, it is important to know the connected power data for each house in the case study location. The connected power data as samples for each of these houses can be seen in the following table.

Table 1 House Connected Power

No	Customer ID	House Code	Power Connected (VA)
1.	523082975871	1	450
2.	523082975895	2	450
3.	523082975894	3	450
4.	523082975893	4	450
5.	523082975892	D	450
6.	523082975879	E	900
7.	523082975845	F	450
8.	523082975812	G	450
9.	523082975803	Н	450
10.	523082975804	I	450

In addition to the connected power, it is also necessary to conduct research related to the service voltage to consumers in the existing network. The service voltage measurement was carried out on May 5, 2020. After obtaining permission from the local RT head, a study was conducted at the case study location by measuring the service voltage at peak load times, which is between 19.00 WIB and outside peak load at 12.00 WIB. The following table 2 shows the results of the measurement of service voltage in the 10 sample houses in the case study locations.

Table 2 Voltage Measurement Results

No	Customer ID	Voltage at Peak Load	Voltage at outside the Peak Load
1.	1	223 Volt	224 Volt
2.	2	221 Volt	223 Volt

3.	3	217 Volt	216 Volt
4.	4	193 Volt	197 Volt
5.	D	183 Volt	192 Volt
6.	E	179 Volt	186 Volt
7.	F	168 Volt	183 Volt
8.	G	163 Volt	180 Volt
9.	H	156 Volt	175 Volt
10.	I	154 Volt	173 Volt

#### 2.5 Modeling of Existing Network Circuits

From Figure 1 regarding the condition of the existing network, circuit modeling can be made to make it easier to simulate the measurement of voltage drop and electrical power losses through calculation formulas or through simulation calculations with the ETAP program.



Figure 2 Existing Network Circuit Modeling

## III. Result and Analysis

## 3.1 Arrangement of Line of Customer Home Connections

This arrangement of house connections (SR) for the customer line is the main point in the repair plan at the case study location. The SR series arrangement is depicted with a red line according to Figure 4.3 below. This SR series arrangement is in accordance with the standards set by PLN that one JTR pole with a maximum of five customer service connections and one customer service connection can be connected in series with a maximum of five customers, as in Figure 3. That way, voltage drops and losses will be obtained on the connection house that fits the standard.

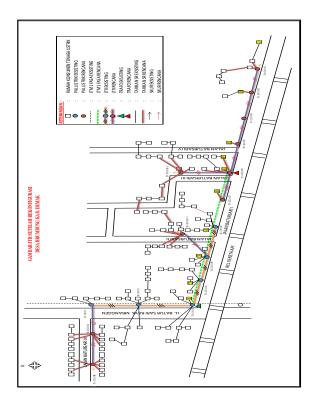


Figure 3 Kondisi Jaringan Setelah Rekonfigurasi

## 3.2 Feasibility Study for Network Reconfiguration Using ETAP Simulation

Feasibility Study on Voltage Drop

The simulations of the feasibility of service voltages using ETAP 12.6.0 software are the same as the ETAP software simulations carried out previously on the existing network of case study locations. The method of drawing poles and buses will also be carried out the same as the simulation of the existing network. The loading factor is assumed to be the same as the loading when the stress measurement is carried out at the case study location. So that with the same loading model, the network repair plan can be known for the voltage drop.

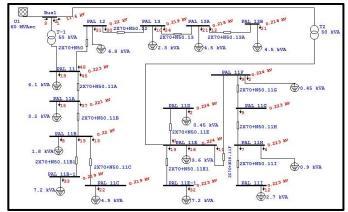


Figure 4 Service Voltage After Reconfiguration with ETAP Simulation

From the simulation results above, a voltage table can be made in each house along with the percentage of voltage drop generated in the network repair plan. For the percentage of voltage drop, it is obtained from a formula such as calculating the percentage of voltage drop in the previous existing network, namely

$$\Delta V (\%) = \frac{Vs - Vr}{Vs} \times 100\%$$

Table 3 Home Voltage ETAP Simulation results

No	House Code	Voltage (Volt)	Voltage Drop Percentage (%)
1.	1	223	0,8
2.	2	221	1,7
3.	3	220	2,2
4.	4	219	2,6
5.	D	224	0,4
6.	Е	224	0,4
7.	F	224	0,4
8.	G	223	0,8
9.	Н	223	0,8
10.	I	223	0,8

## 3.3 Feasibility Study on Shrinkage

The power loss feasibility study uses the same method as the voltage drop feasibility study above. The power loss feasibility study uses a simulation with ETAP 12.6 software with data in accordance with the network reconfiguration that has been planned in the previous section. The following are the results of the power loss simulation using ETAP 12.6 software:

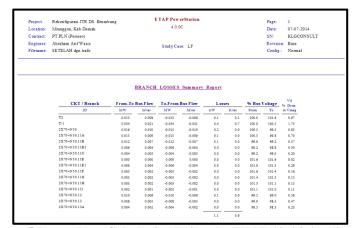


Figure 5 Power Loss Calculation Using the ETAP 12.6.0 Application

From the results of the power loss calculations on ETAP 12.6 according to Figure 4.5 above, it is known that the total power loss in the network after reconfiguration is 1,100 Watts. However, because the author does not discuss transformer losses, the shrinkage will only be 600 Watt, because it is reduced by 500 Watt transformer losses. If used as a percentage, the percentage of power loss in the network regardless of transformer losses is 1.3%.

**Table 4 Comparison of Total Power Loss** 

No.	Power Loss		Power Loss After	
	Before Reconfiguration		Reconfiguration	
1.	3.900 Watt	8,3 %	600 Watt.	1,3 %

It can be seen in Table 4, after reconfiguring the network, the amount of power loss has decreased to 1.3% and has met the applicable standards.

IV. CONCLUSION

Before the network reconfiguration was carried out, the magnitude of the voltage drop in Brumbung Village was 0.8% - 31.5% and the power loss was 8%, this was not in accordance with the standards set by PT PLN (Persero).

Planning for network reconfiguration in Brumbung Village includes the addition of 10 new poles to get consumers closer to the voltage source, enlarging the size of the network cable, expanding the 1-phase Medium Voltage Network, adding a 50KVA 1-phase distribution transformer, and reconfiguring Home Connections.

After reconfiguring the network, the magnitude of the voltage drop according to the ETAP simulation, the voltage drop is 0.4% - 2.6% and the power loss is 1.1%, these results are in accordance with SPLN No.1: 1995 for a maximum voltage drop of 10% and SPLN 72: 1987 for power losses (losses) a maximum of 3.5%.

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