

# Laser Induced Breakdown Spectroscopy for Identification & Quantification of Elemental Composition of Steel Structures: A Study of Early Stage Rust Behaviour in Steel

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**Abstract-** The investigation of the signal intensity and plasma temperature parameters involved with steel structures experiencing early stage rust are described. A simple laboratory set-up involving a ruby laser, mirror, focusing lens, collecting optics and a miniaturised spectrometer were used to conduct the experiments. The spectra from the first two shots on the rust steel sample correlates to that of the rust layers where Carbon (C) was the only sensitive element detected. However, the significant presence of C in subsequent shots could be as a result or a combination of: material alteration due to the rust layer, presence of the analyte line in both the layer and underlying bulk material; and residual rust particles still present in the crater or perimeter of the ablation region. Investigating the temperature parameter for both the rust layer and regular surface showed no significant distinction in the values.

## I. INTRODUCTION

Laser Induced Breakdown Spectroscopy (LIBS) is a useful technique for material characterisation in terms of elemental composition and quantification. Because of its relatively fast measurement, LIBS can be used for real time, *in situ* analysis without the hassle of exporting the target sample back to the laboratory. Furthermore, LIBS is suitable for non-destructive and non-invasive testing of materials since a small amount of mass and surface area is usually interrogated by the laser. LIBS for field applications require no elaborate equipment set-up and sample preparation [1-10].

LIBS analysis of steel mainly involves the identification of atomic constituents of the sample and with useful calibration standards, determining its concentration (quantitative/semi-quantitative analysis). Rust layers on steel often indicate the presence of iron oxides [1-7] [11-16].

For qualitative analysis, identifying the element emissions in air due to higher ionised species ( $>10\text{eV}$ ) could be difficult because electron-ion recombination (to form neutrals) occurs early due to the restricted plasma expansion [1] [3] [7] [17-18]. As the ambient pressure decreases in air (after the laser shot), the plasma lifetime also decreases due to less trapping and recycling of the absorbed energy in the plasma volume thus species with higher ionisation potential will have recombined with free electrons in the cooling plasma [1-3] [5-6] [19]. In vacuum, the plasma expands freely away from the surface with the ions, electrons, atoms/molecules (ejecta) expanding at different

speeds, thus recombination process occurs at a much latter stage as opposed to air [7]. In water, there is even more difficulty as the plasma exhibits strong plasma confinement and quenching effects making the lifetime of the plasma too short and presence of highly ionised species unlikely. The resulting spectrum is typically dominated by intense background light with little spectroscopic information and broadened emission lines due to the high optical density of the plasma. In some cases, only major elements from ablated samples can be detected. Poor signal output can be attributed to the thermal conductivity, density and incompressible nature of water. Also, majority of the pulse energy after absorption losses is used to create vapour cavity on the solid surface with little or no energy used for excitation purposes [10] [19-38]. However, LIBS signals from rust steel underwater are somewhat low and the ablated particles reduce the water transparency for subsequent laser shots [36].

Yao et al. studied and compared the plasma parameters (line intensity, temperature and ablated crater) of different microstructures from a single steel sample to discriminate pearlitic/ferritic from martensitic phases [39]. AbdelKareem et al. investigated the rust and regular surfaces of metal threads with copper as the main component. Converging results were acquired from LIBS and EDX (Energy- Dispersive X-Ray Spectroscopy) analysis on the clean surface; but LIBS could not detect some elements such as Chlorine and Sulphur when interrogating rust surfaces [18]. Nasrazadani and Namduri also studied the phase transformation in iron oxides. Linear correlation procedures compared the samples to commercial iron oxide powders where correlation values of close to one were achieved [15]. Boue-Bigné extended LIBS applications for fast micro-analysis technique to monitor segregation and decarburisation for improved quality of the final product in the steel manufacturing industry. Concentration maps showed the presence of segregation elements and decarburisation layers [14]. Kim et al. developed a portable LIBS system to monitor paints and coatings using peak picking and correlation algorithms. They were able to obtain matches of above 90% with reference paint samples [40]. Ardakani and Tavassoli conducted depth profile analyses of coated and attached layers on steel and aluminium substrates where their interfacial parameters showed no effects on laser ablation. Using normalised intensity for interface position is not entirely accurate as it depends on plasma temperature and pulse energy. Normalised concentration provided better depth resolution in comparison [41]. Hemmerlin

et al. analysed steel samples using Vacuum Ultraviolet LIBS and compared results with Spark Discharge-Optical Emission Spectroscopy (SD-OES) [42]. Similar sensitivities were obtained for identifying elements of interest related to process control in steel manufacturing. SD-OES showed better Limits of Detection (LOD) in agreement with [18].

Carbon steel as an engineering material accounts for a great percentage of steel production worldwide even with its limited corrosion resistance. It is used in nuclear and fossil fuel power plants, transportation, marine, petroleum production and refining, pipelines, chemical processing, metal processing, mining and construction. In an event where carbon steel is exposed to moist air or a thin film of water, rust formation can accelerate further in an atmosphere containing gaseous atmospheric constituent capable of strong electrolytic activity.

In hazardous areas where physical access is not possible, LIBS can be a useful tool for *in situ* analysis on steel structures experiencing early stage (I/II) rust; providing single shot spectroscopic information from repetitive sampling at the same location to interrogate both the non-uniform surface and underlying bulk composition. This paper aims to investigate signal intensity as well as plasma temperature parameters of rust steel and identify analyte elements from the surface alteration due to early stage rust.

about 3.75  $\mu\text{s}$ . The hollow cylindrically shaped mild steel sample was interrogated with single laser shots and the resulting spectra recorded. 10 individual laser shots were fired on the sample's regular and rust surface to maintain consistency in comparison. Carbon steel Certified Reference Material (CRM) was to compare variations of the regular surface's analyte signal.

## II. EXPERIMENTAL

Ruby laser of wavelength, pulse width and repetition rate of 694.3 nm, 50 ns, 0.1 Hz respectively were used to interrogate the sample. The pulse energy was kept relatively stable at about 30 mJ through the experiments. The pulse energy level prevented excess material ablation on the rust layer particularly after the first laser pulse and allowed for proper shot-to-shot material analysis.

The laser pulse was directed to the sample via a ruby 45° mirror and 110 mm UV fused silica lens. The collecting optics compacted in an optical cage consisted of:

- Thor labs LB4592 UV fused silica bi-convex uncoated lens with focal length ( $f= 60$  mm), diameter ( $\varnothing=50.8$  mm)
- Thor labs LB4821 UV fused silica bi-convex uncoated lens with focal length ( $f= 100$  mm), diameter ( $\varnothing=50.8$  mm)
- Short-pass filter placed between the LB4821 lens and the fibre optic probe to cut-off wavelength above 650 nm, preventing both signal intensity saturation and potential damage of the fibre optic cable

The 600  $\mu\text{m}$  core diameter fibre optic cable was positioned at the end of the cage to collect and transmit plasma light to the entrance slit of the ocean optics USB 2000+ spectrometer with the integration time set to 1ms. The flashlamp of the laser was internally triggered with a Q-switch delay of 1200  $\mu\text{s}$ . To resolve the spectral window against background light and for optimum signal, the pulse generator was used to adjust the delay (to about 1200  $\mu\text{s}$ ) between the flashlamp sync pulse and output trigger pulse to the spectrometer. The measured spectrometer delay was



Fig 1. Mild Steel sample showing rust layer and regular surface sections

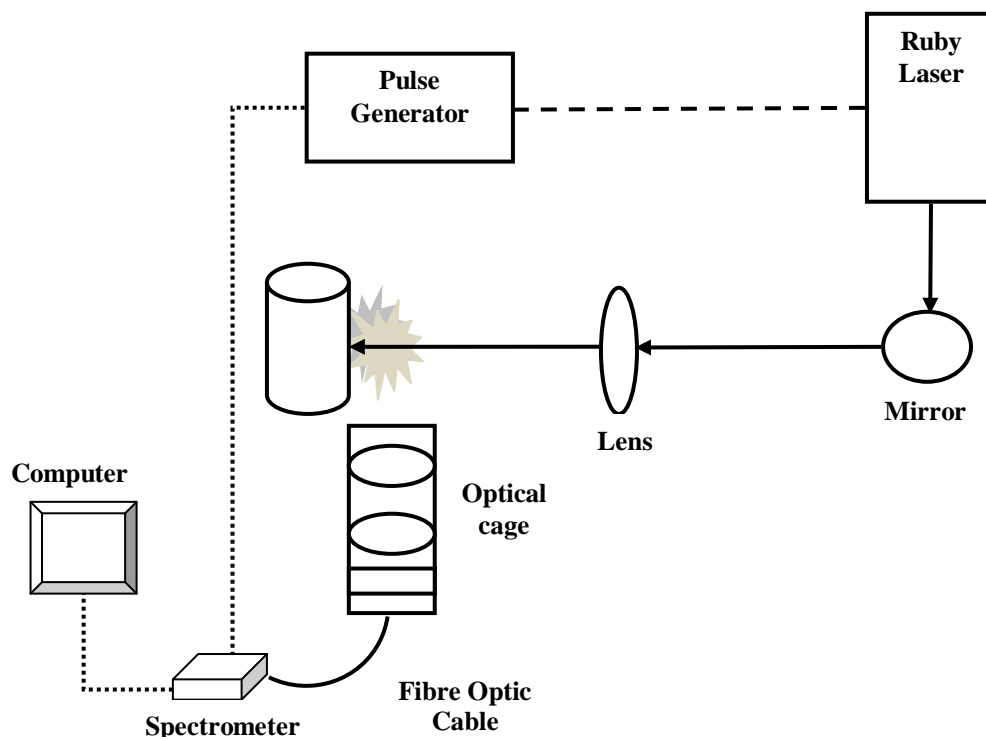


Fig 2. Laboratory based LIBS set-up

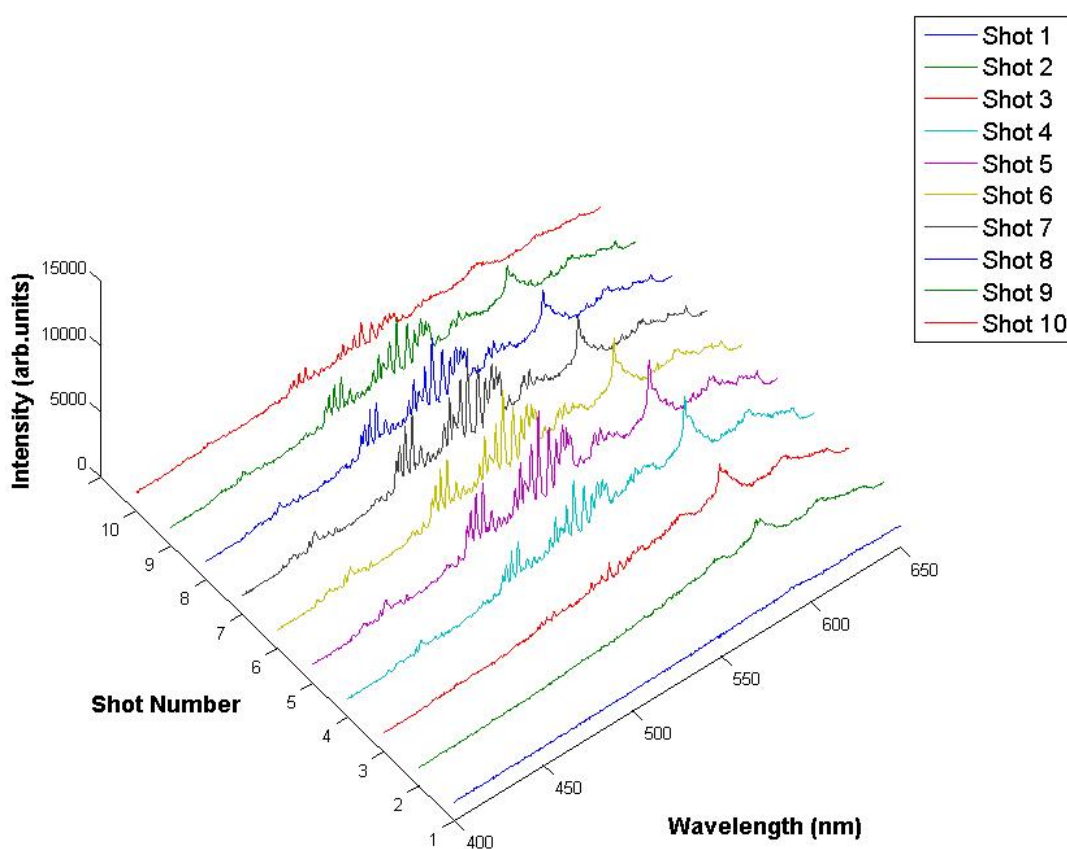
### III. RESULTS AND DISCUSSION

The first 2 shots on the rust layer show the absence of the sensitive bulk matrix [Fe (I)] lines within the spectral

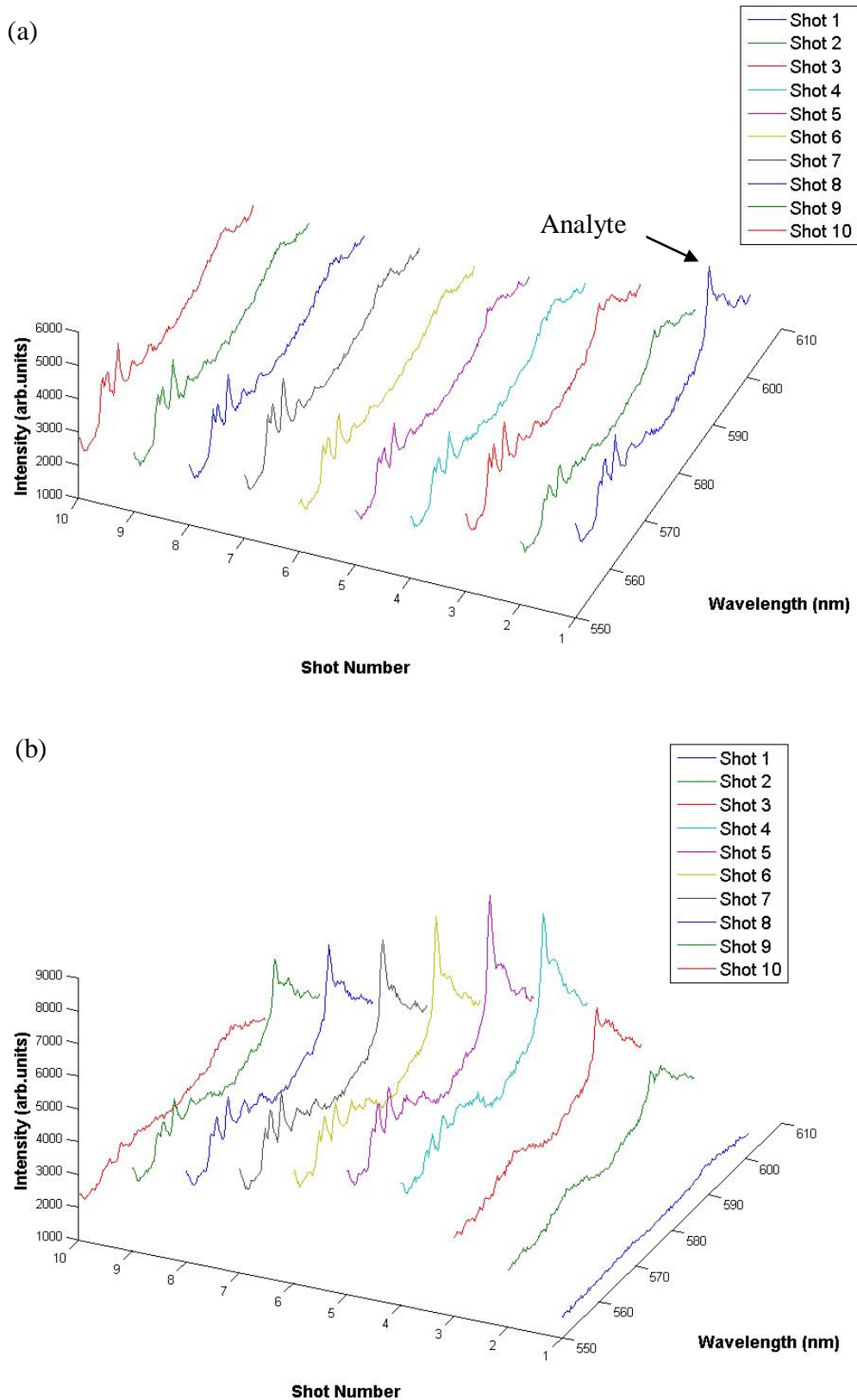
window which could only be observed clearly from the 4<sup>th</sup> shot onwards after more layer ablation and interrogation of

the bulk composition (Figure 3). This could imply that the spectra from the initial two shots depicts to a level, the characteristics of the rust layer. Although the first shot yields no meaningful spectroscopic information, the second shot shows the presence of the 588.9 nm analyte (C) line. From the 4<sup>th</sup> to 10<sup>th</sup> shot where sensitive bulk matrix lines appear, the analyte line is still persistent with significant intensity. This indicates the analyte is present in

both the layer and underlying bulk material. Comparing with the spectra from the regular surface (Figure 4a), the analyte line is only significant in the first shot but no clear observations in subsequent shots as the lines appear indistinct. Figure 5 shows the intensity variations of the analyte and bulk matrix lines with shot number for the regular surface and rust layer.



**Fig 3. LIBS spectra obtained from the rust layer section over 10 shots**



**Fig 4 LIBS spectra obtained from regular surface (a) and rust layer (b) section highlighting the analyte line variations with shot number**

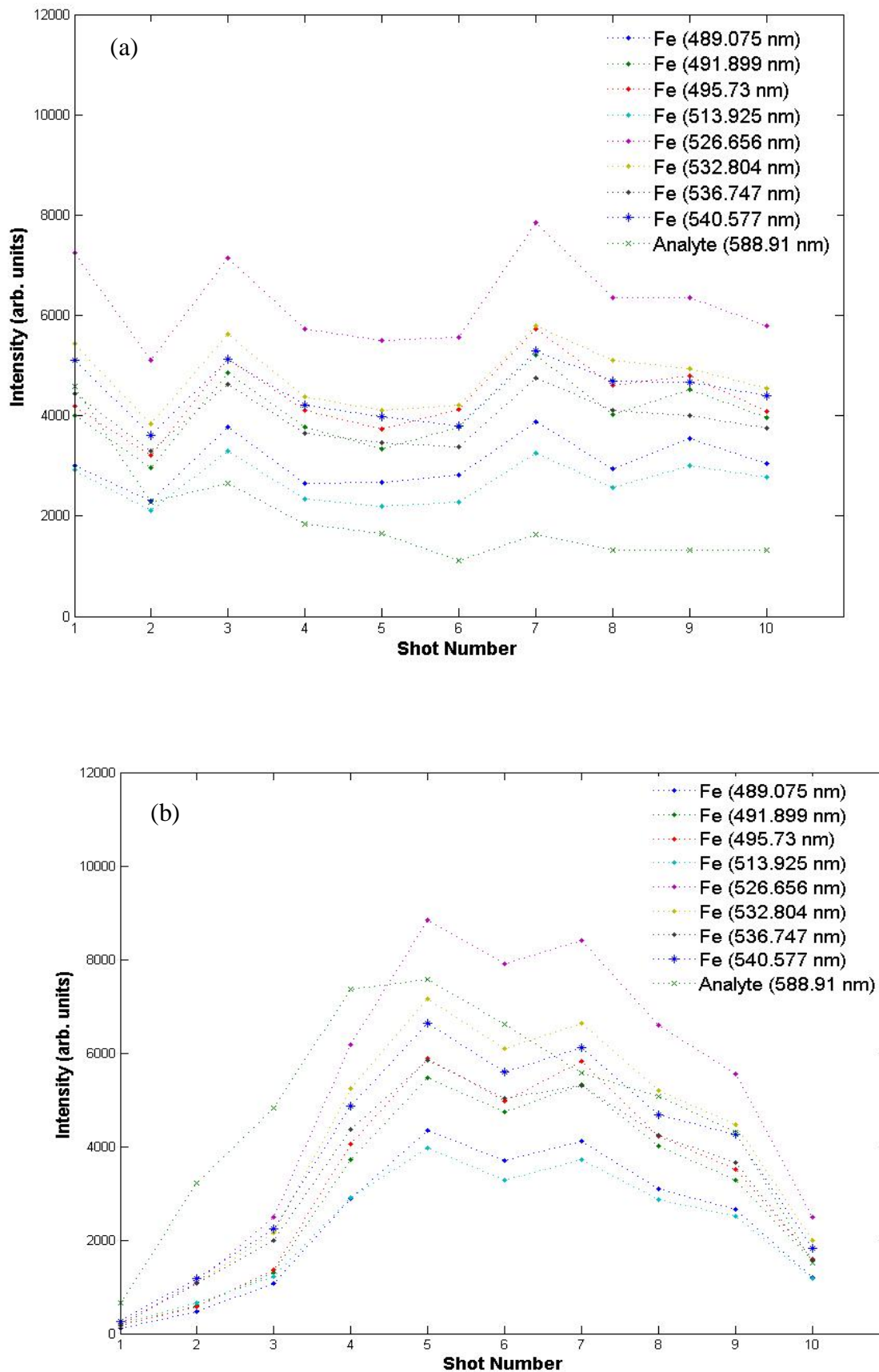
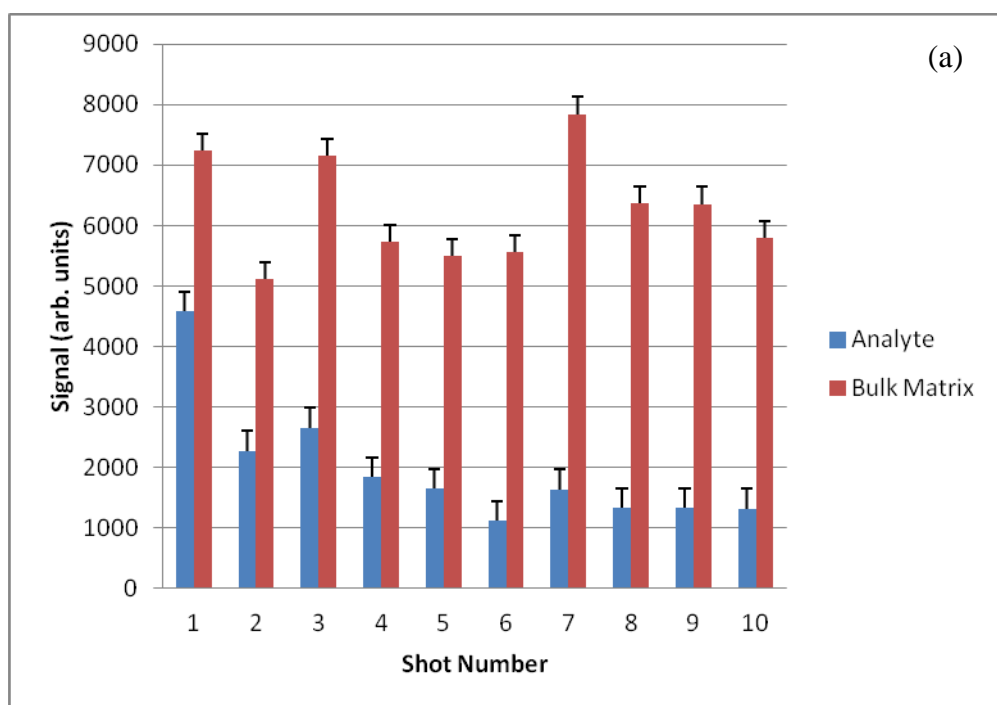
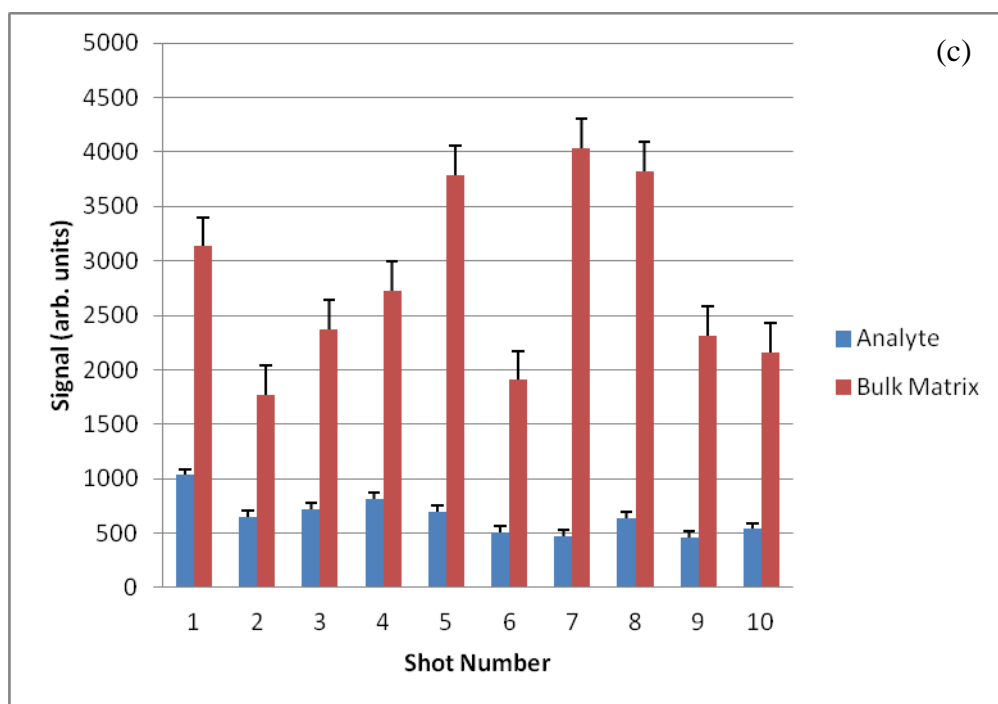
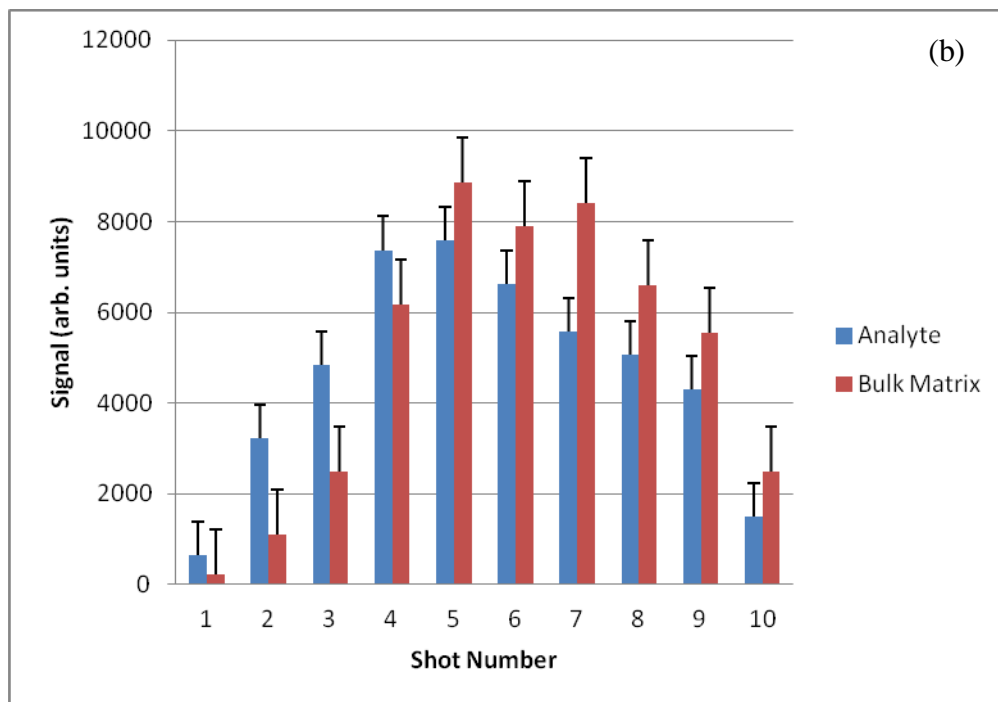


Fig 5. Signal Intensity variation with shot number for analyte and bulk matrix lines [(a) regular surface, (b) rust layer]

The contrast in the analyte line intensity behaviour could be attributed to the layer characteristics. The rust layer spectra observation shows similarities to interrogating a layered material; except in this case, a particular analyte line sensitivity relating to the layer composition still persists after layer ablation. To further validate the results seen in figure 5, the most sensitive Fe bulk matrix line (526.65 nm) and the analyte line signals were investigated for the carbon steel sample (regular surface and rust layer) and compared with the CRM sample – carbon steel (Figure 6). The standard error bars were inserted to acknowledge shot-to-shot plasma variation from the single laser shots. The CRM sample containing 0.598 % C; shows similarities to the regular surface of the test carbon steel sample in terms of the

variation trend in the analyte signals. Although, the CRM shows a better measure of signal repeatability as seen in the lower error bars (Figure 6c). Greater error bars in the measured analyte signal observed in figure 6b could be attributed to the surface non-uniformity from the rust process. The presence of useful quantity carbon in the rust layer spectra could be as a result of the presence of iron carbide in the steel structure and the subsequent leaching with Fe to form solutions in the event of rust. In steel, none of carbon is present on its own as it is all dissolved in the iron as part of the microstructures during manufacturing. Depending on the stage, rust process could produce a new and less desirable material from the original steel product. However, these deductions will have to be validated with further experiments.





**Fig 6. Signal Intensity variation with shot number for analyte and bulk matrix line (Fe/526.65 nm) [(a) regular surface, (b) rust layer, (c) CRM - Carbon Steel]**

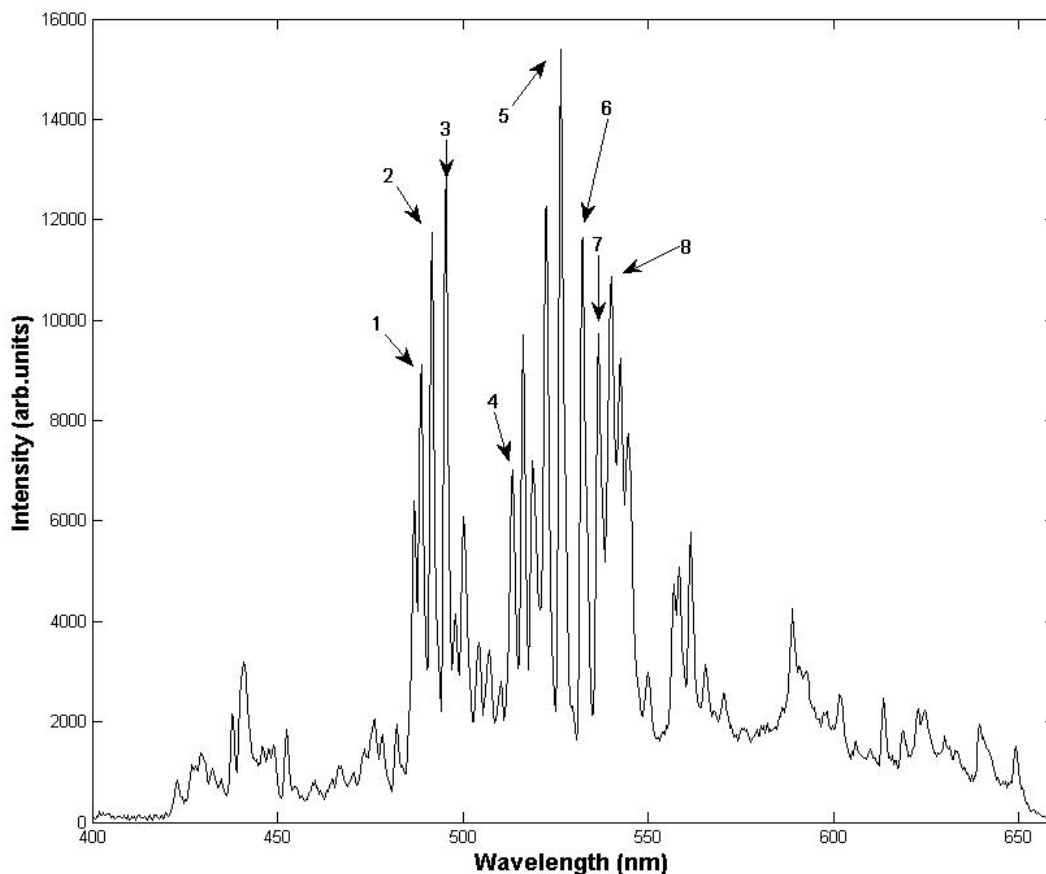
8 bulk matrix Fe lines (ranging from 488 nm to 540 nm) were selected and its intensity variation investigated and compared with the analyte line (C) for both rust layer and regular surface as shown in figure 5. The selected lines

were subsequently used for Boltzmann plot to measure the temperature and observe a similar variation for each shot. The plasma temperature calculated from each plot is dependent on experimental parameters such as the time



delay, integration time (gate width) and measured signal intensity. The slope ( $eV^{-1}$ ) of the linear plot and the Boltzmann constant ( $eV/K$ ) were used to determine the

Boltzmann temperature. Table 1 shows the temperature and slope results from the Boltzmann plots.



**Fig 7. Selected Fe lines used for Boltzmann plot to measure the plasma temperature**

**Table 1 Plasma temperature results generated from the Boltzmann plots.**

	Temperature			Slope		
	Value (K)	Accuracy Error (%)	Standard Error (K)	Value ( $eV^{-1}$ )	Accuracy Error (%)	Standard Error ( $eV^{-1}$ )
Regular Surface	$7976 \pm 57$	0.7	$\pm 18$	$-1.455 \pm 0.01$	0.7	$\pm 0.003$
Rust Layer	$7886 \pm 75$	0.95	$\pm 24$	$-1.4716 \pm 0.014$	0.96	$\pm 0.004$
CRM – carbon Steel	$7882 \pm 86$	1.1	$\pm 27$	$-1.4724 \pm 0.016$	1.1	$\pm 0.005$

Temperature variations relating to the Regular surface, Rust Layer and CRM for each shot are shown in figure 8. There is no significant distinction as observed in the signal intensity investigation. Under the same experimental conditions, the rust layer showed the highest mean temperature value over 10 shots. The results in table 1 validate the experimental accuracy of LIBS for single shot interrogation because of the accuracy errors (not greater than 1.1 %). The calculated plasma temperature relies strongly on the slope of the Boltzmann plots and thus, temperature accuracy is also dependent on the standard error of the slope. Values of intercept in Boltzmann plots are rarely used to validate the accuracy of the measured plasma temperature. To ensure some sort of reliability of using temperature measurements to characterise the rust sample using LIBS, approximations must be adopted to define the plasma state.

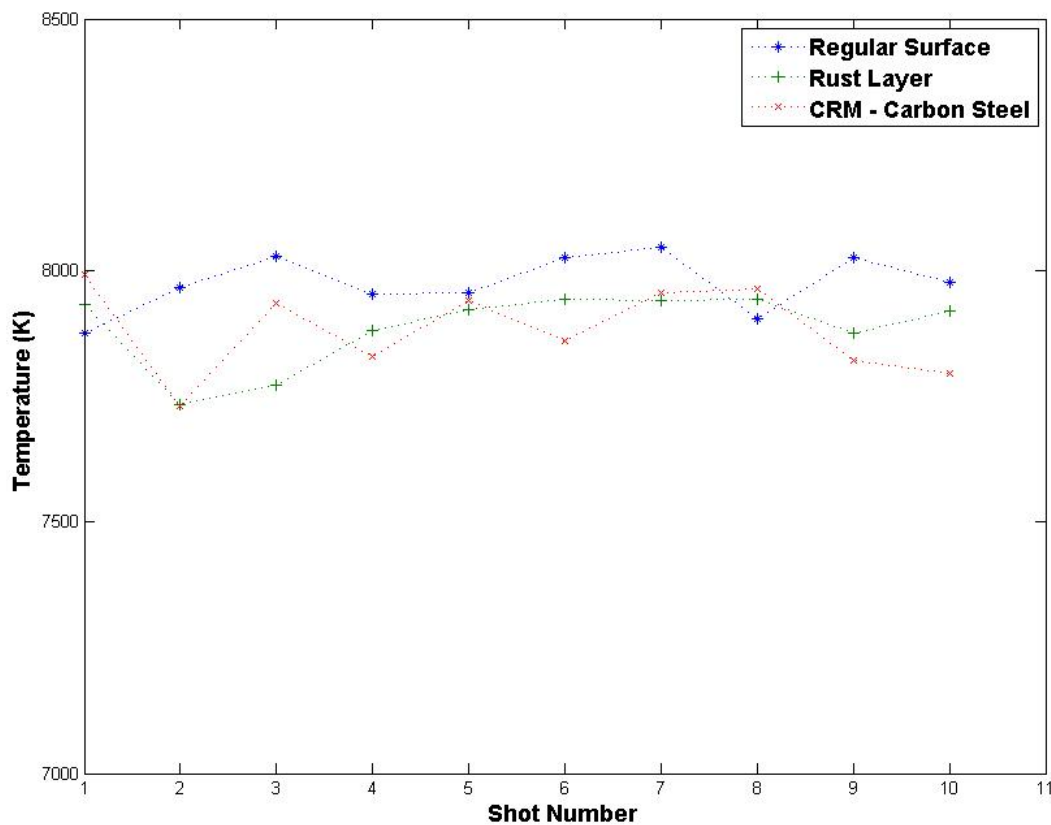


Fig 8. Temperature variation with shot number for the clean surface and rust layer sections

#### IV. CONCLUSION

LIBS usefulness as a method to interrogate rust metals lies on its repeatability, invasiveness, accessibility and analytical power. The spectra from the first two shots on the carbon steel sample correlates to that of the rust layers where C was the only sensitive element detected. However, the significant presence of C in subsequent shots could be as a result or a combination of: material alteration with respect to the bulk composition owing to the rust layer, presence of the analyte line in both the layer and

underlying bulk material and residual rust particles still present in the crater of the ablated region. Investigating temperature variation with shots for both rust and clean surface did not result greatly in distinguishing rust layer characteristics.

Results from studying fundamental intensity and temperature parameters validate to confident degree, LIBS as a fast, real-time, *in situ* analytical tool for providing spectroscopic information from repetitive sampling.

Further work will involve:

- Studying the effects of the presence of the underlying bulk material of steel on LIBS signal related to the rust layer.
- Studying the effects of pulse energy on spectra analysis relating to bulk matrix and analyte signal intensity; and investigating what pulse energy range has the most reduced influence on bulk matrix and analyte signal interaction.
- Investigating the effects of rust layer and underlying bulk composition have in identifying higher ionised elements of interest (notably Fe).

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